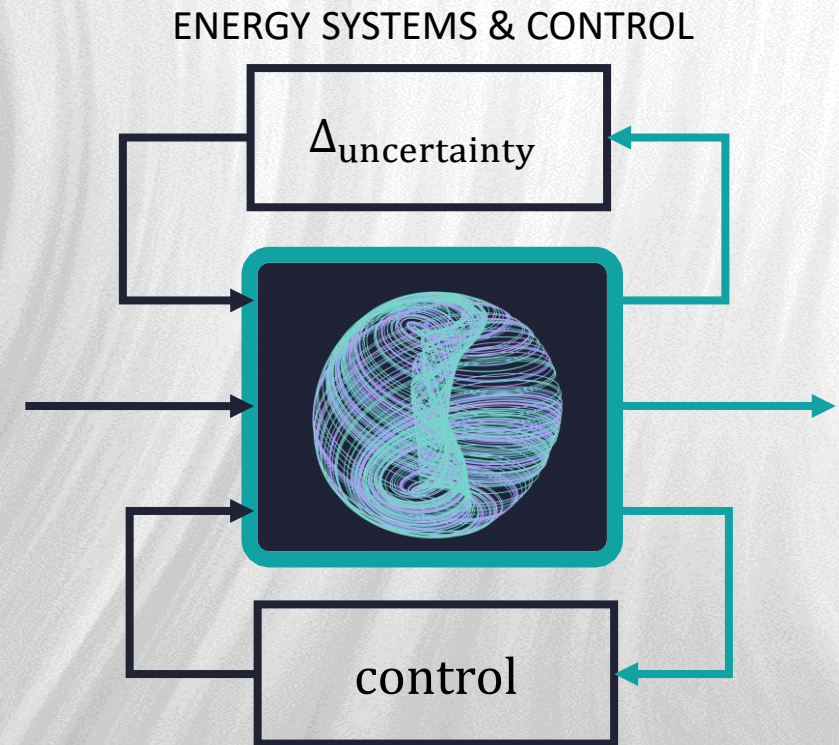
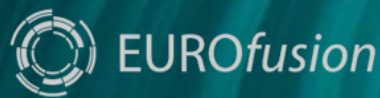


Applying self-consistent electron heat transport and ECH deposition profile estimation in DIII-D

27th Joint EU-US Transport Task Force Meeting

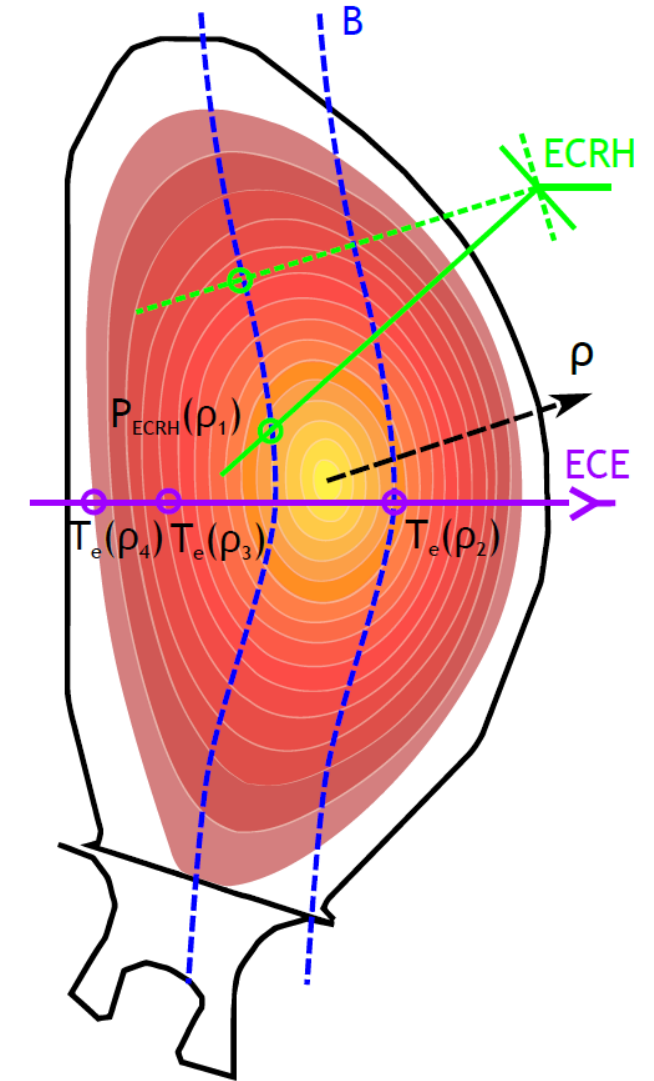
Jelle Slief

R.J.R. van Kampen, B.F.H. van den Boorn, M.W. Brookman, E. Westerhof, M. van Berkel



Introduction

- Transport is often studied **perturbatively**^[1-5]
- **Power deposition** and **transport** estimates are traditionally separated
- However, **edge turbulence** can spoil deposition localization^[6-10]
- Need for **simultaneous, self-consistent estimate** of transport coefficients and power deposition profile^[6,10-13]



[1] J.D. Callen *et al.* (1977). *Phys. Rev. Lett.* **38** 491-4

[2] H.J. Hatfuss *et al.* (1994). *Plasma Phys. Control. Fusion*. **36** B17-B37

[3] N.J. Lopes Cardozo. (1995). *Plasma Phys. Control. Fusion*. **37** 799

[4] F. Ryter *et al.* (2010). *Plasma Phys. Control. Fusion*. **52** 124043

[5] C.C. Petty *et al.* (2015). *Nucl. Fusion*. **55** 083011

[6] K.K. Kirov *et al.* (2002). *Plasma Phys. Control. Fusion*. **44** 2583

[7] C. Tsironis *et al.* (2009). *Phys. Plasmas*. **16** 112510

[8] A. Snicker *et al.* (2018). *Nucl. Fusion*. **58** 016002

[9] O. Chellai *et al.* (2021). *Nucl. Fusion*. **61** 066011

[10] M.W. Brookman *et al.* (2023). *Nucl. Fusion*. **63** 044001

[11] E.A. Lerche *et al.* (2008). *Plasma Phys. Control. Fusion*. **50** 035003

[12] A. Manini *et al.* (2003). *Nucl. Fusion*. **43** 490-511

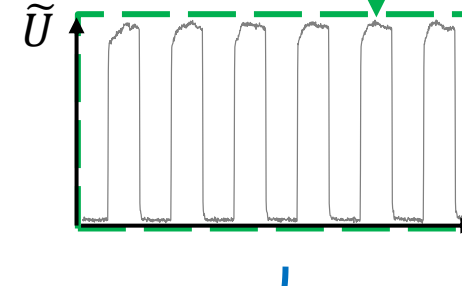
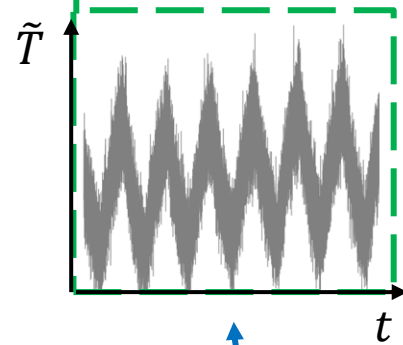
[13] F. Ryter *et al.* (2003) *Nucl. Fusion*. **43** 1396

Outline

- Spatially varying, joint transport and power deposition estimates
- Assumptions and experimental checks
- Sensitivity analysis
- Experimental power deposition estimates in DIII-D
- Impact for ITER

Linearization through perturbative experiments - the model

$$\frac{\partial}{\partial t} \tilde{T}(x, t) = -\nabla \cdot [D(x)\nabla\tilde{T}(x, t) + V(x)\tilde{T}(x, t)] + K(x)\tilde{T}(x, t) + P(x)\tilde{U}(t)$$



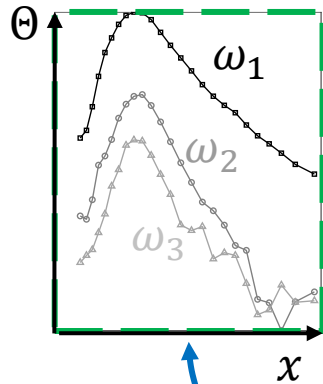
Measured
Temperature perturbation $\tilde{T}(x, t)$
Gradient $\nabla\tilde{T}(x, t)$

Unknown
Diffusivity $D(x)/\chi(x)$
Convectivity $V(x)$
Damping $K(x)/\tau_{inv}(x)$
Power deposition $P(x)$

Measured
Source modulation $\tilde{U}(t)$

Linearization through perturbative experiments - frequency domain

$$i\omega\Theta(x, \omega) = -\nabla \cdot [D(x)\nabla\Theta(x, \omega) + V(x)\Theta(x, \omega)] + K(x)\Theta(x, \omega) + P(x)Y(\omega)$$

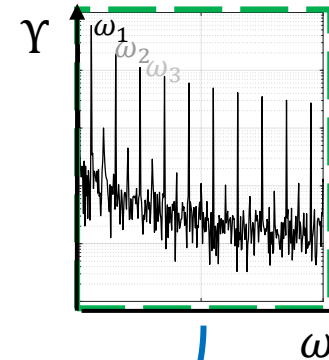


Measured
Temperature perturbation
Gradient

$\Theta(x, \omega)$
 $\nabla\Theta(x, \omega)$

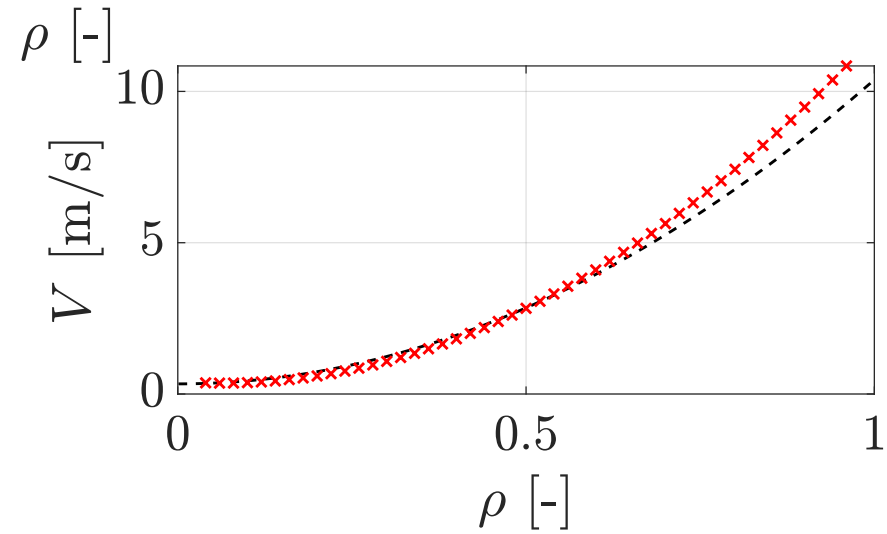
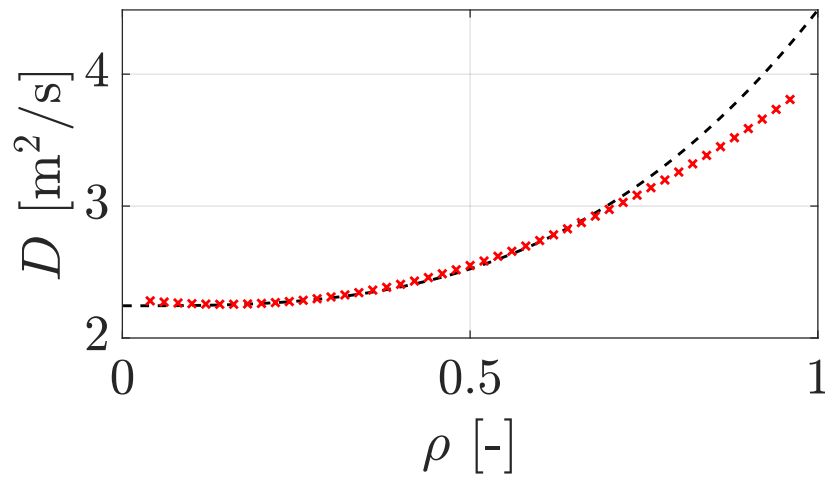
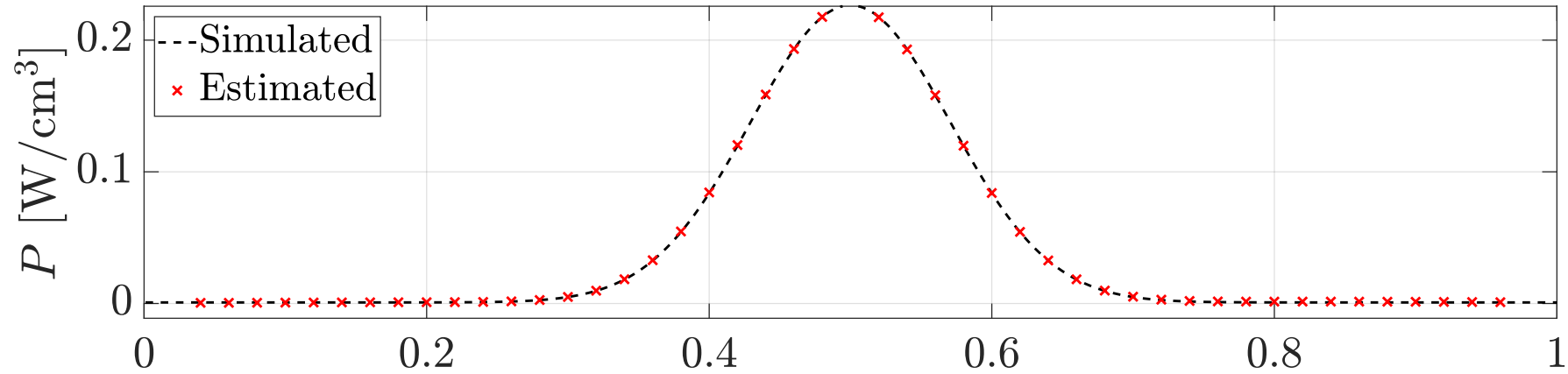
Unknown
Diffusivity
Convectivity
Damping
Power deposition

$D(x)/\chi(x)$
 $V(x)$
 $K(x)/\tau_{inv}(x)$
 $P(x)$



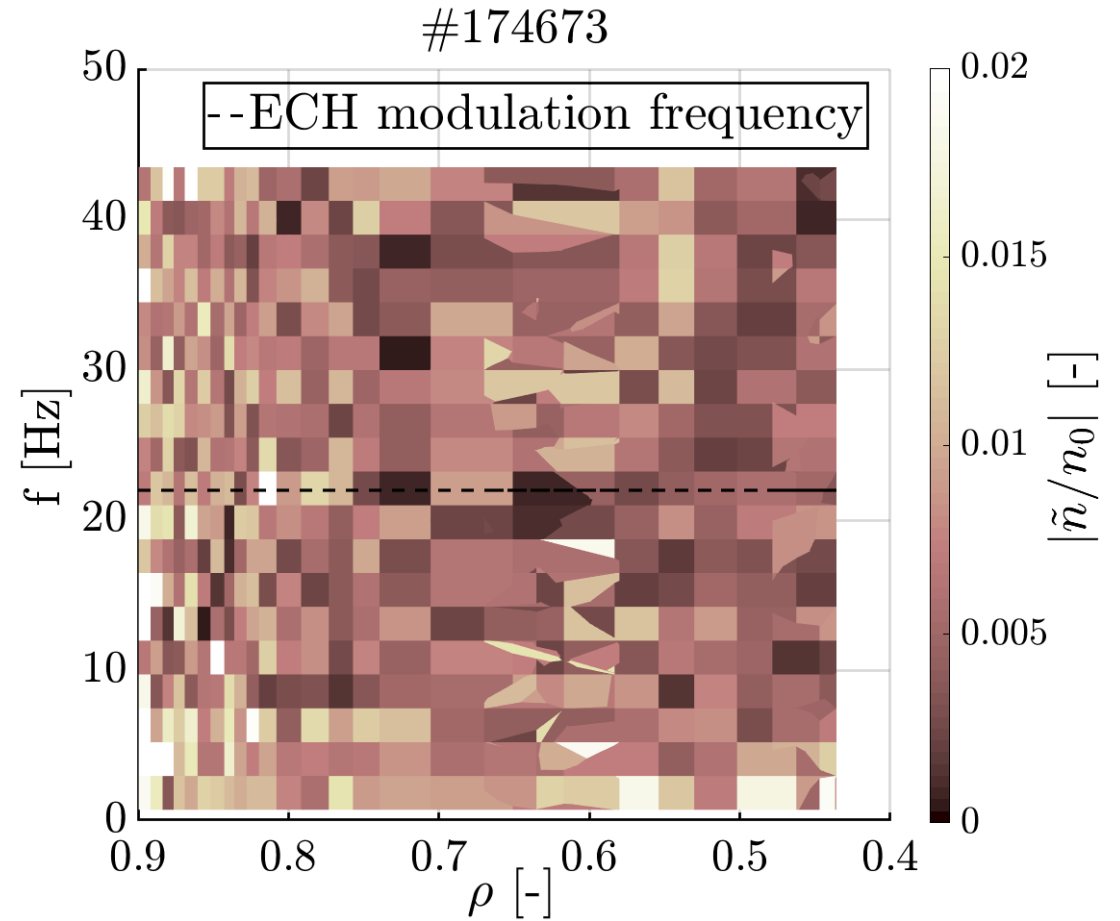
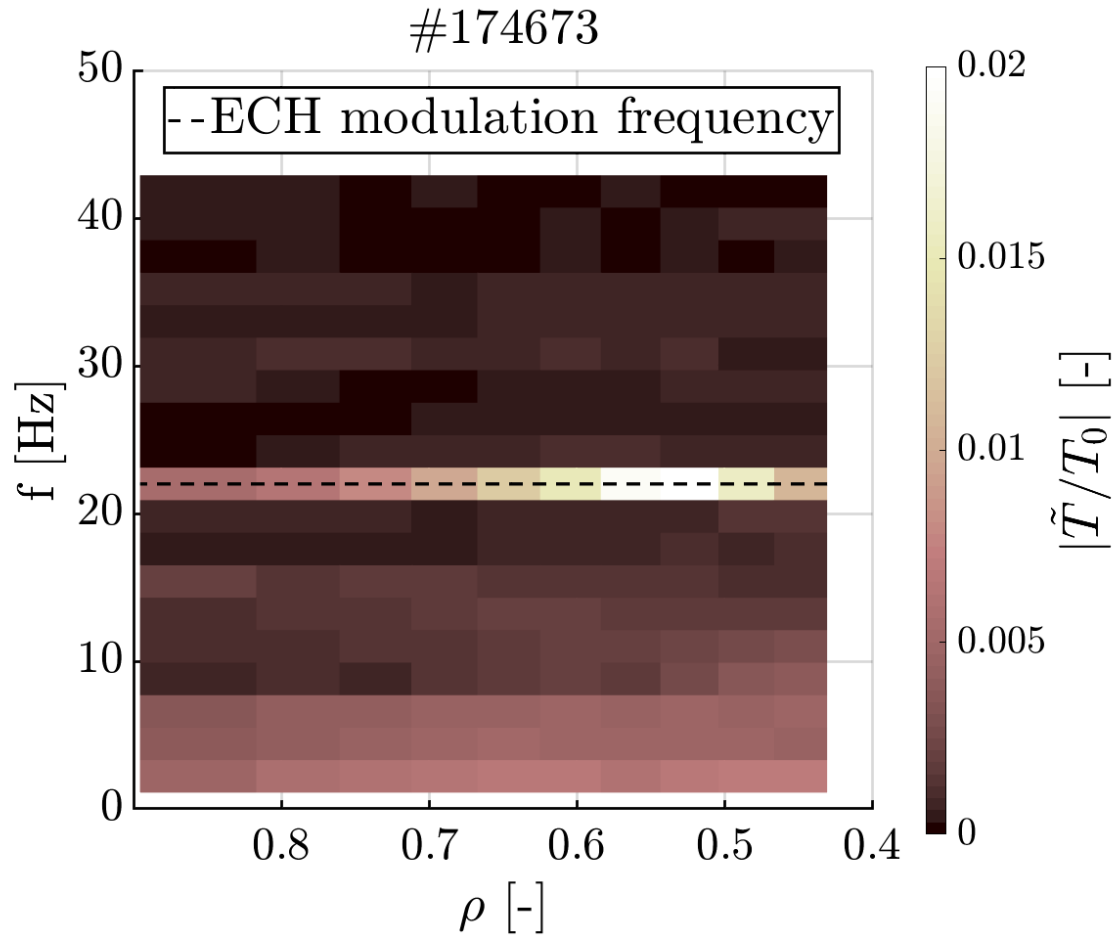
Measured
Source modulation $Y(\omega)$

Estimation



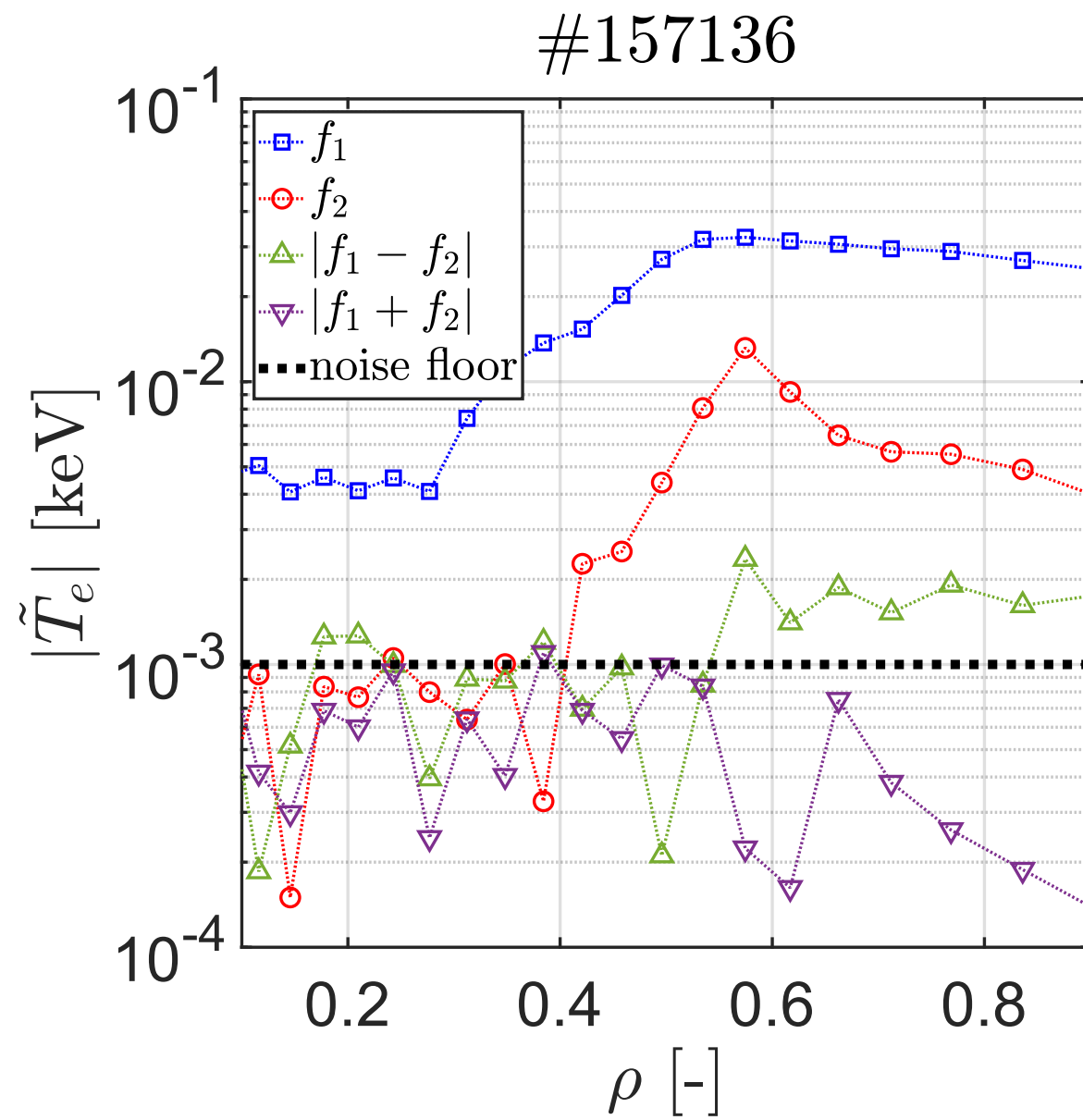
Justification of model assumptions

- Density is not modulated ($\frac{\partial}{\partial t} n_e = 0$)



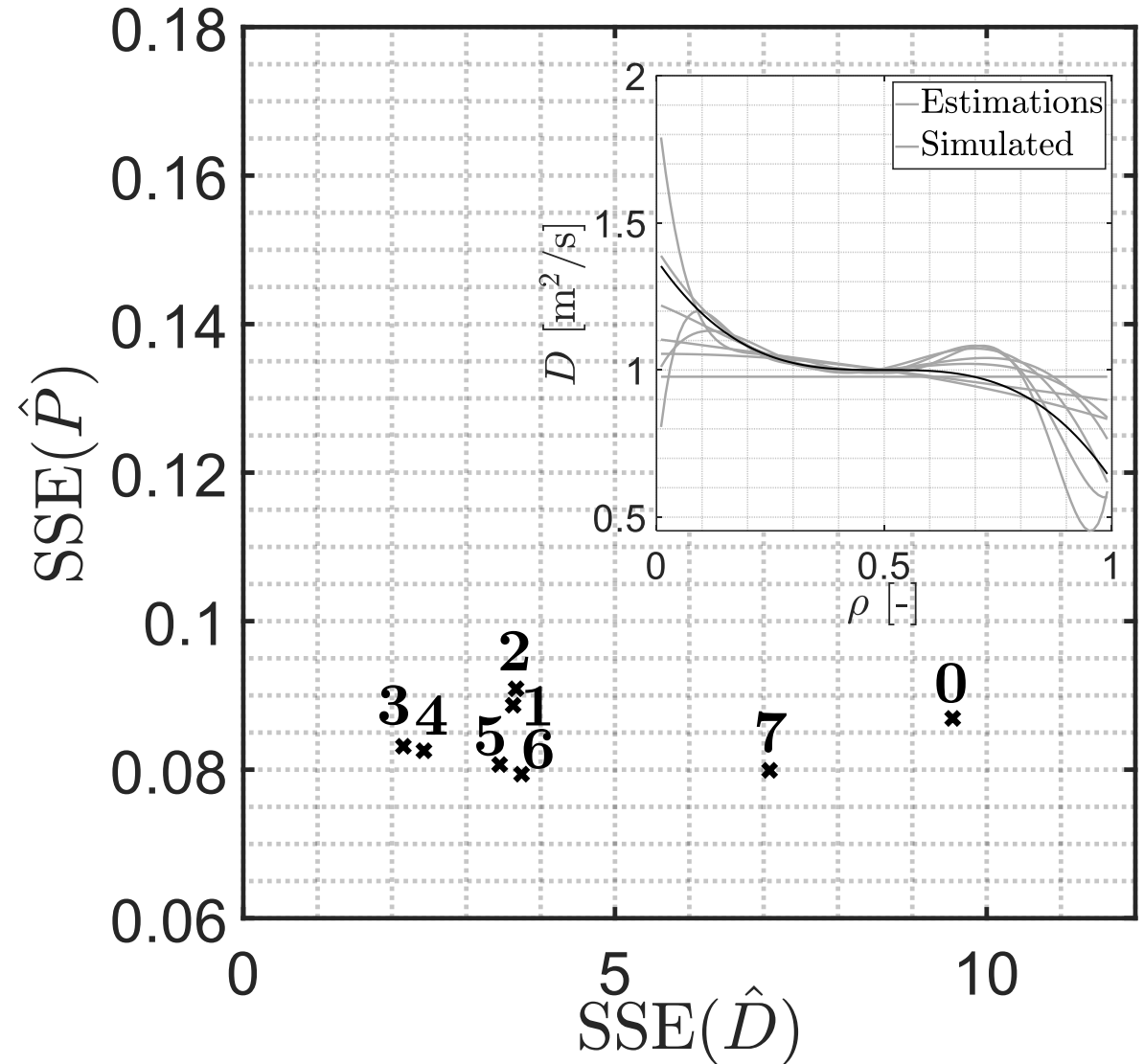
Justification of model assumptions

- Linearity of the plasma response



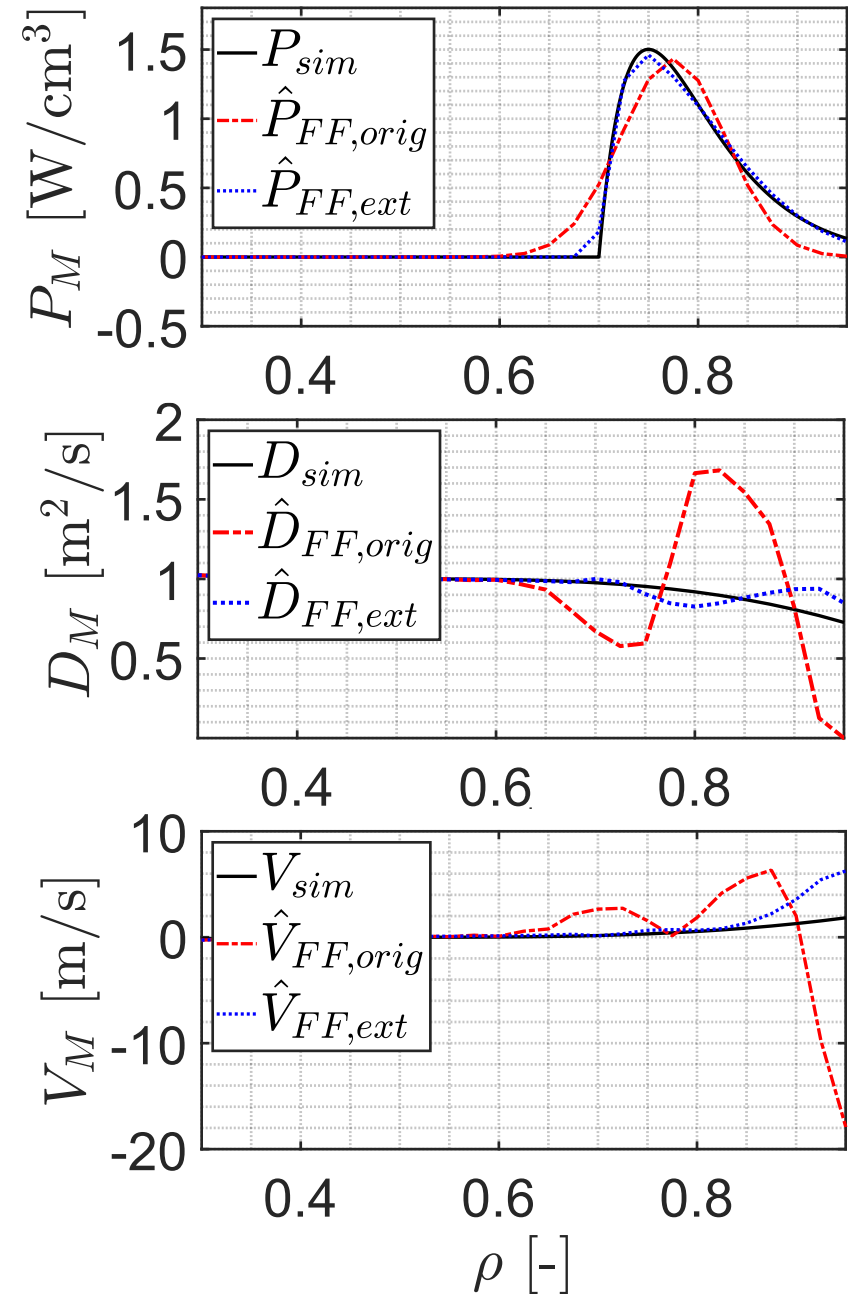
Sensitivity of model coefficients

- Sensitivity of estimates of one parameter to errors in the estimates of others
- Result: **P estimate is insensitive to variations in D and V**



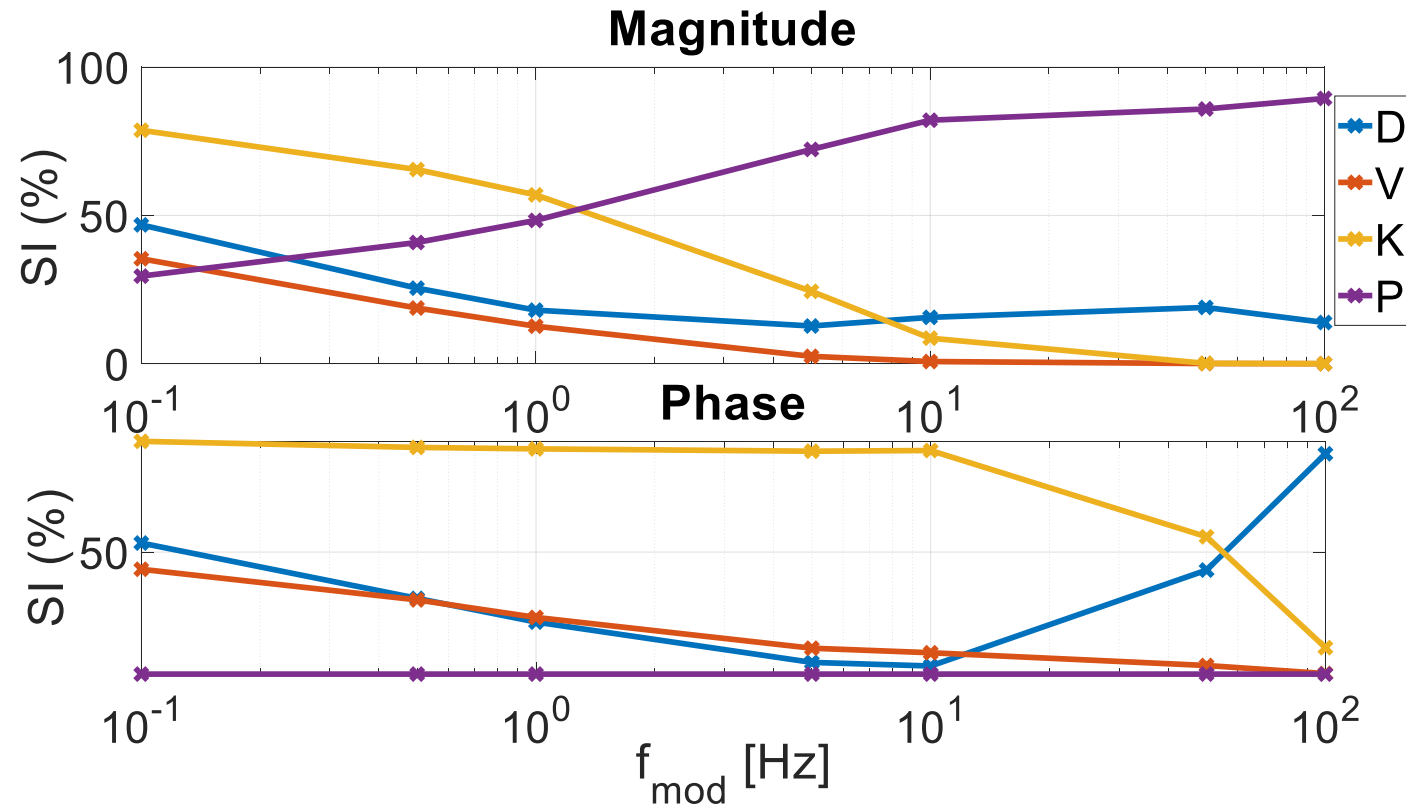
Sensitivity of model coefficients

- Small errors in P get compensated in other parameters
- Large deviations in D and V
- Due to different sensitivity of the temperature profile to different coefficients



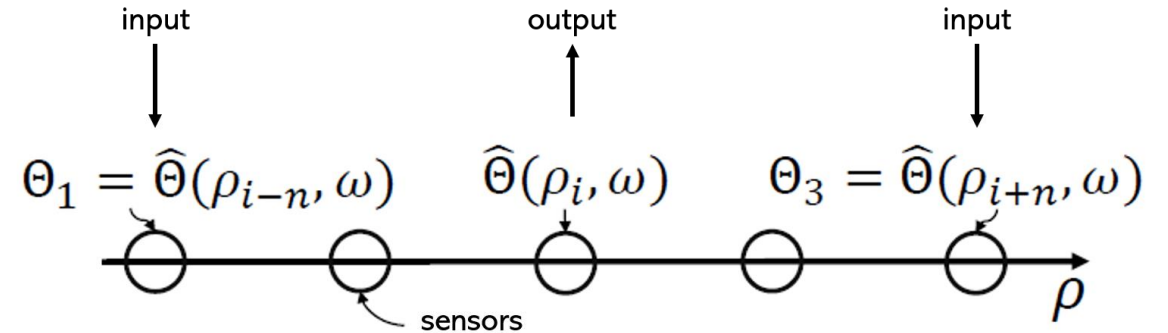
Sensitivity of model coefficients

- Sensitivity of the temperature profile to different parameters under noisy conditions
- **Depends on modulation frequency**
- The effect of **P dominates**
- Future, large devices: more deposition broadening, so joint estimation required
- Depending on the coefficient of interest, *magnitude or phase response* in *different frequency ranges*



Estimation methods: a brief overview

- **Maximum Likelihood Estimator** ^[1] (MLE)
 - Estimate D,V,K,P constant on subdomain
 - Taking noise covariances into account
 - Nonlinear optimization
- **Frequency Domain Least Squares** ^[2] (FDLS)
 - Parametrize spatial dependence of D,V,K,P in terms of basis functions
 - Derive closed-form linear least squares solution for hyperparameters
- **Flux fit** ^[3,4] (FF)
 - Parametrization of P as a modified Gaussian
 - Parametrize heat flux q in terms of D,V as basis functions
 - Fit the flux term to the deposition term using nonlinear optimization
- **Break-in-slope** ^[5] (BIS)
 - Trusted method, used as reference
 - Time-domain, no transport
 - Requires step in power; deposition proportional to break in temperature slope



[1] M. Van Berkel *et al.* (2014). *Automatica*. **50**. 2113–2119.

[2] R. J. R. van Kampen, *et al.* (2020). *IEEE Control Syst. Lett.* **5**. 1681-1686.

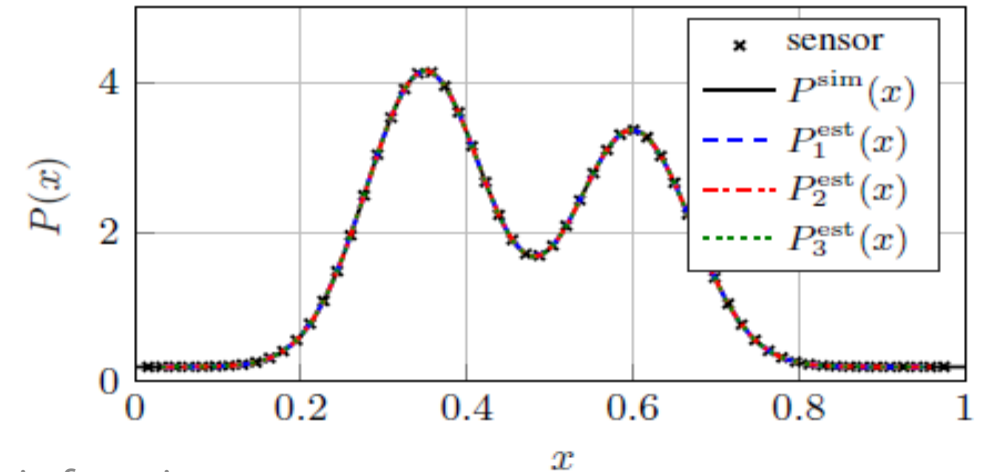
[3] M. W. Brookman *et al.* (2021). *Phys. Plasmas*. **28**. 42507.

[4] Slief *et al.* (2022). *Phys. Plasmas*. **29**. 010703.

[5] E.A. Lerche *et al.* (2008). *Plasma Phys. Control. Fusion*. **50** 035003

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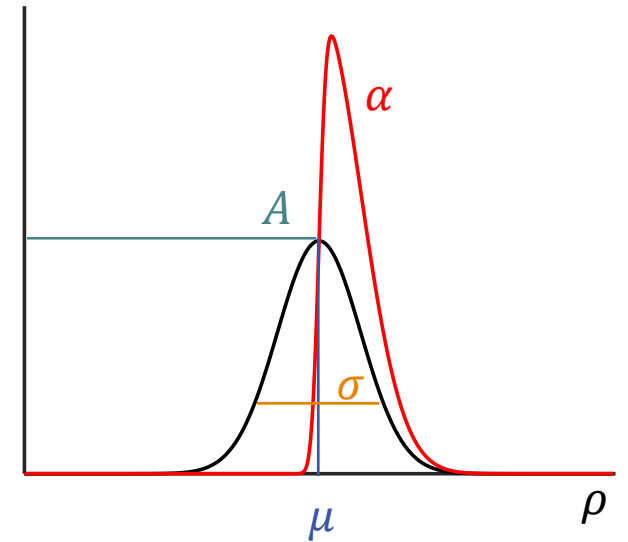
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$$\tilde{q}_e(\rho, \omega) = \frac{1}{\rho} \int_0^1 \rho' \left(P(\rho', \sigma, \mu, A, \alpha) \tilde{U}(\omega) - \frac{3}{2} n_e(\rho') i\omega \Theta(\rho', \omega) \right) d\rho'$$

- Break-in-slope ^[5] (BIS)

- Trusted method, used as reference
- Time-domain, no transport
- Requires step in power; deposition proportional to break in temperature slope

$$\tilde{q}_e(\rho, \omega) = -D(\rho) n_e(\rho) \frac{\partial \Theta}{\partial \rho}(\rho, \omega) + V(\rho) n_e(\rho) \Theta(\rho, \omega)$$



[1] M. Van Berkel *et al.* (2014). *Automatica*. **50**. 2113–2119.

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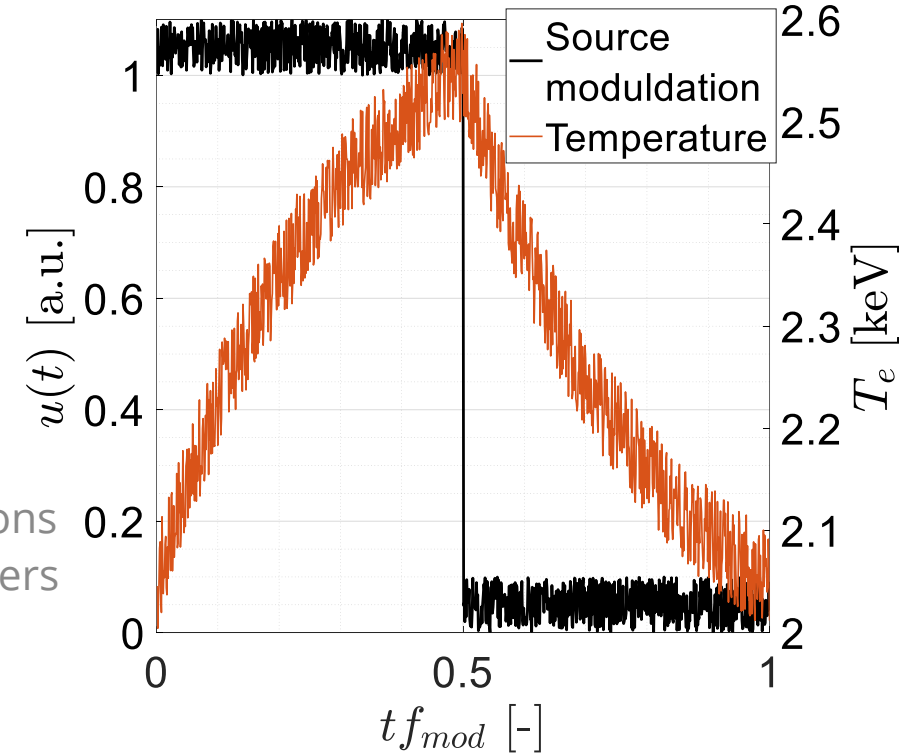
[3] M. W. Brookman *et al.* (2021). *Phys. Plasmas*. **28**. 42507.

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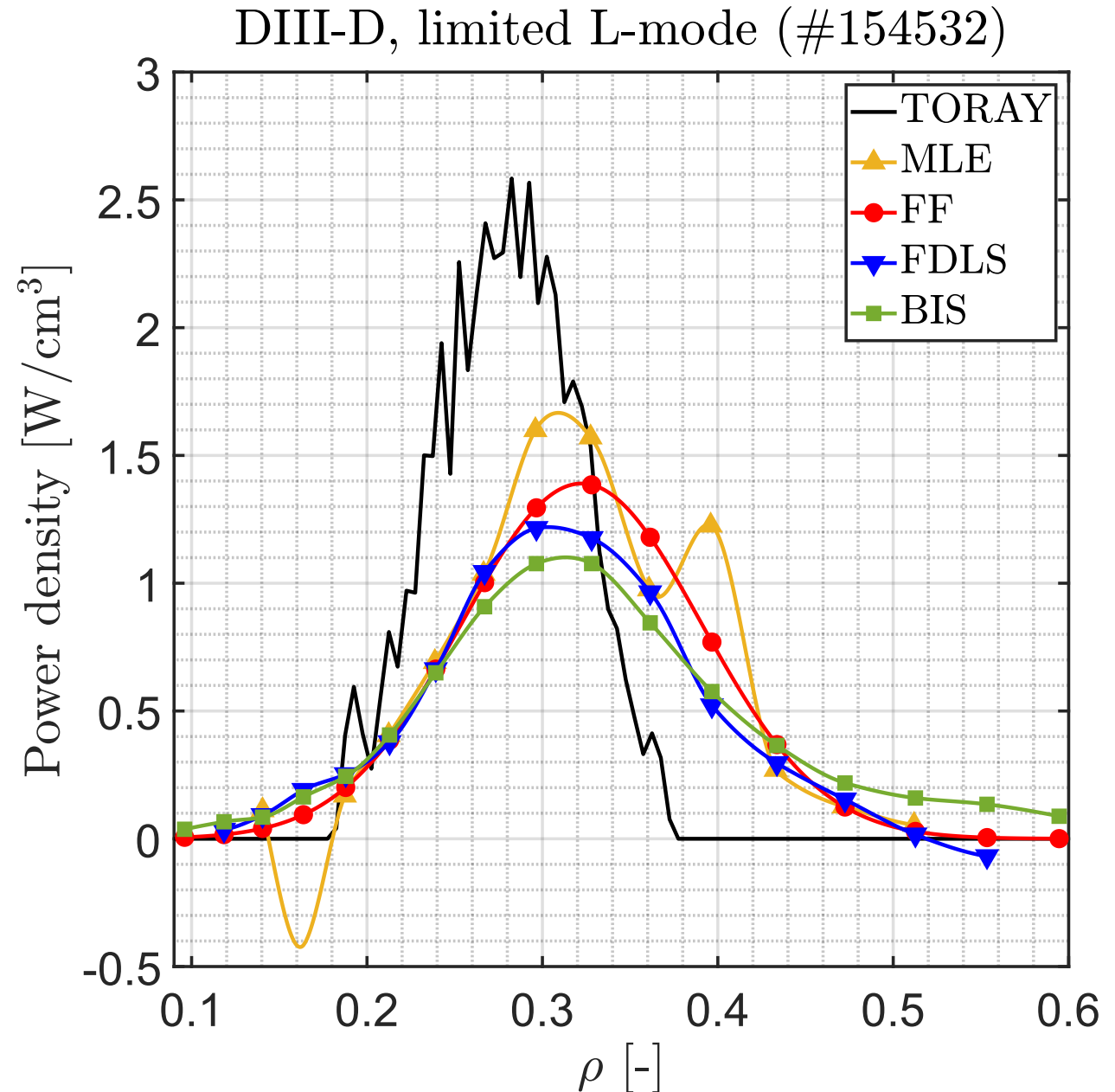
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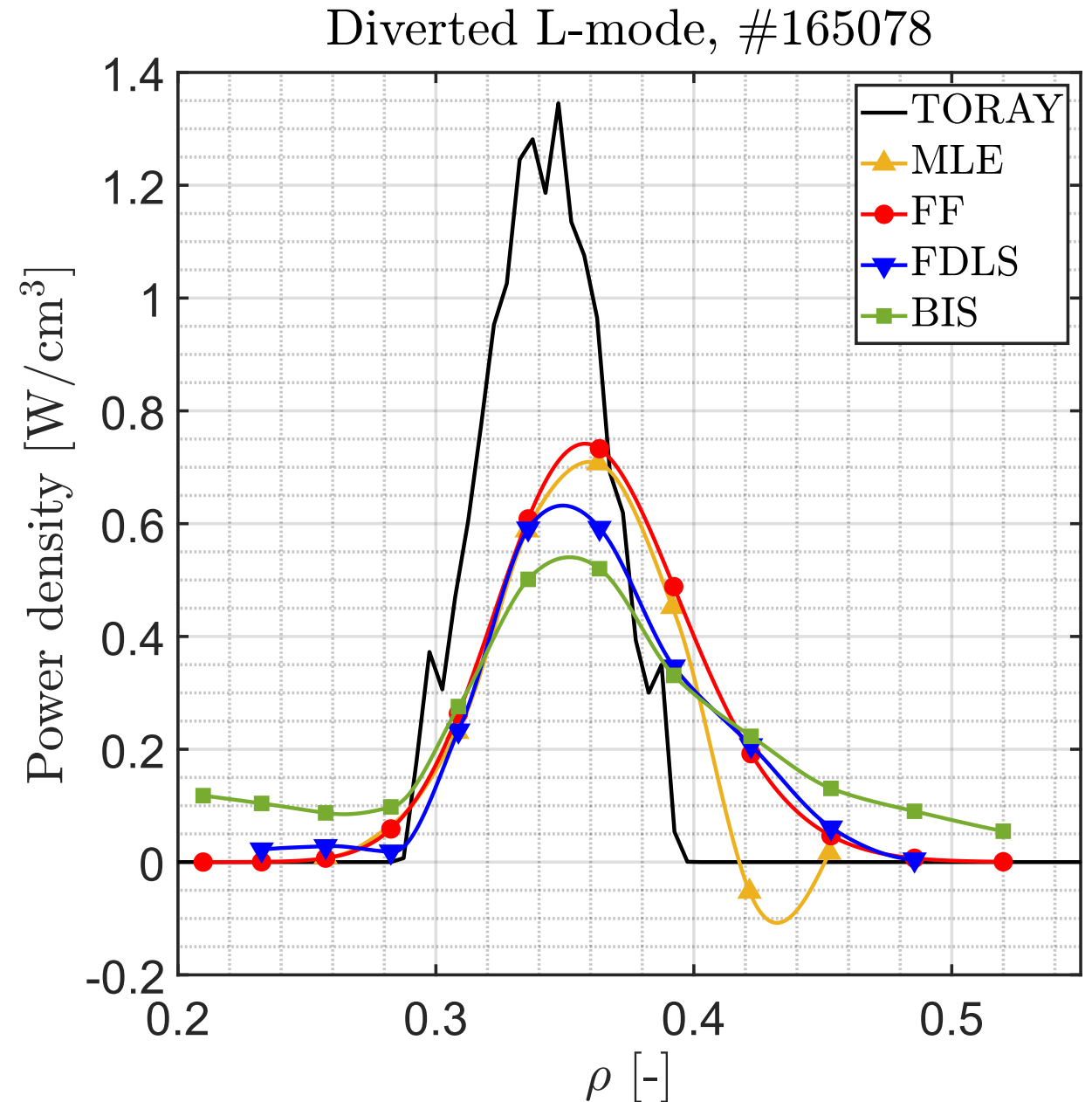
Results – DIII-D

- Estimation of P in DIII-D: factor 1.5 – 3 broadening with respect to ray-tracing^[1]
- Broad agreement between different experimental methods



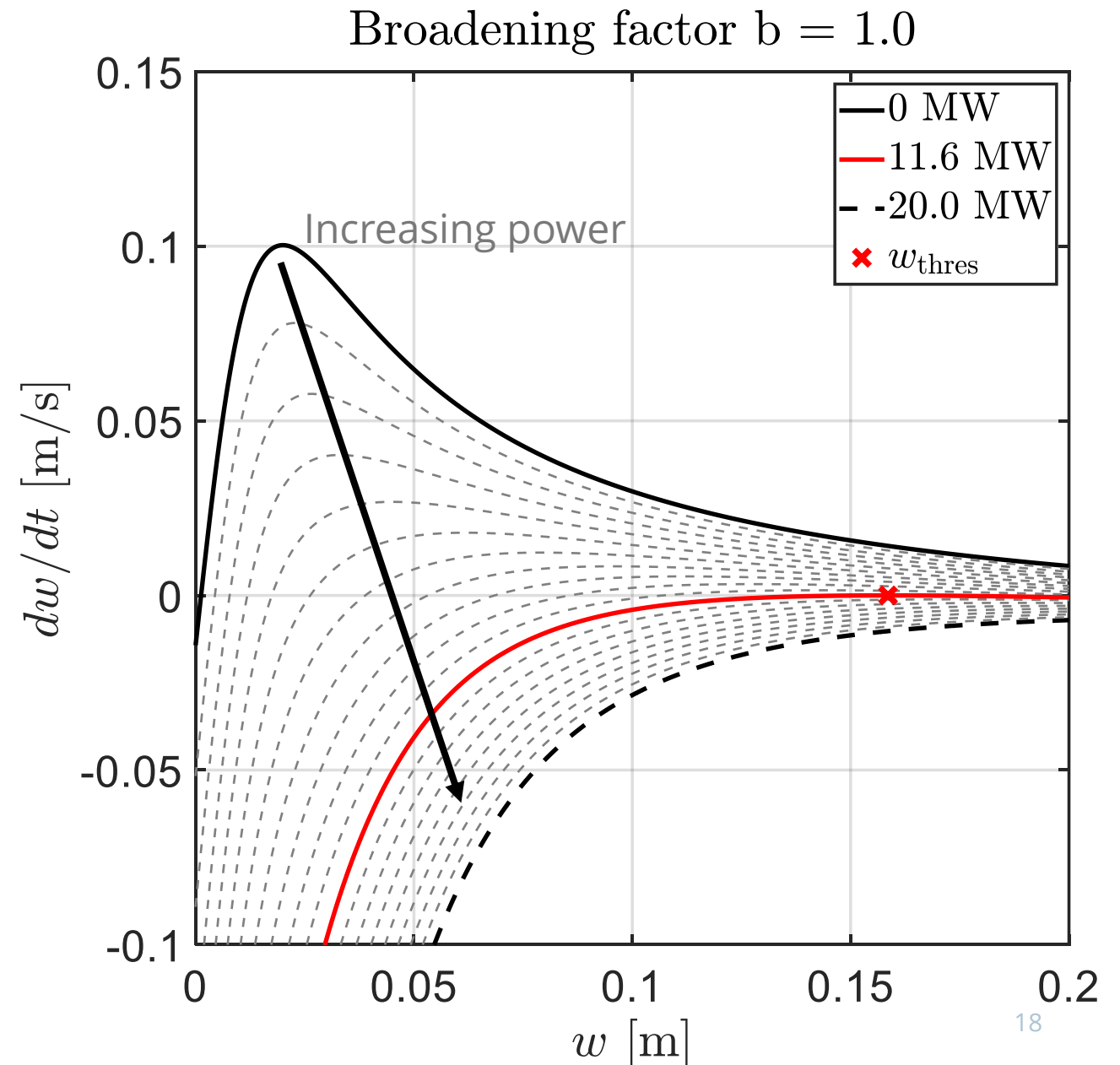
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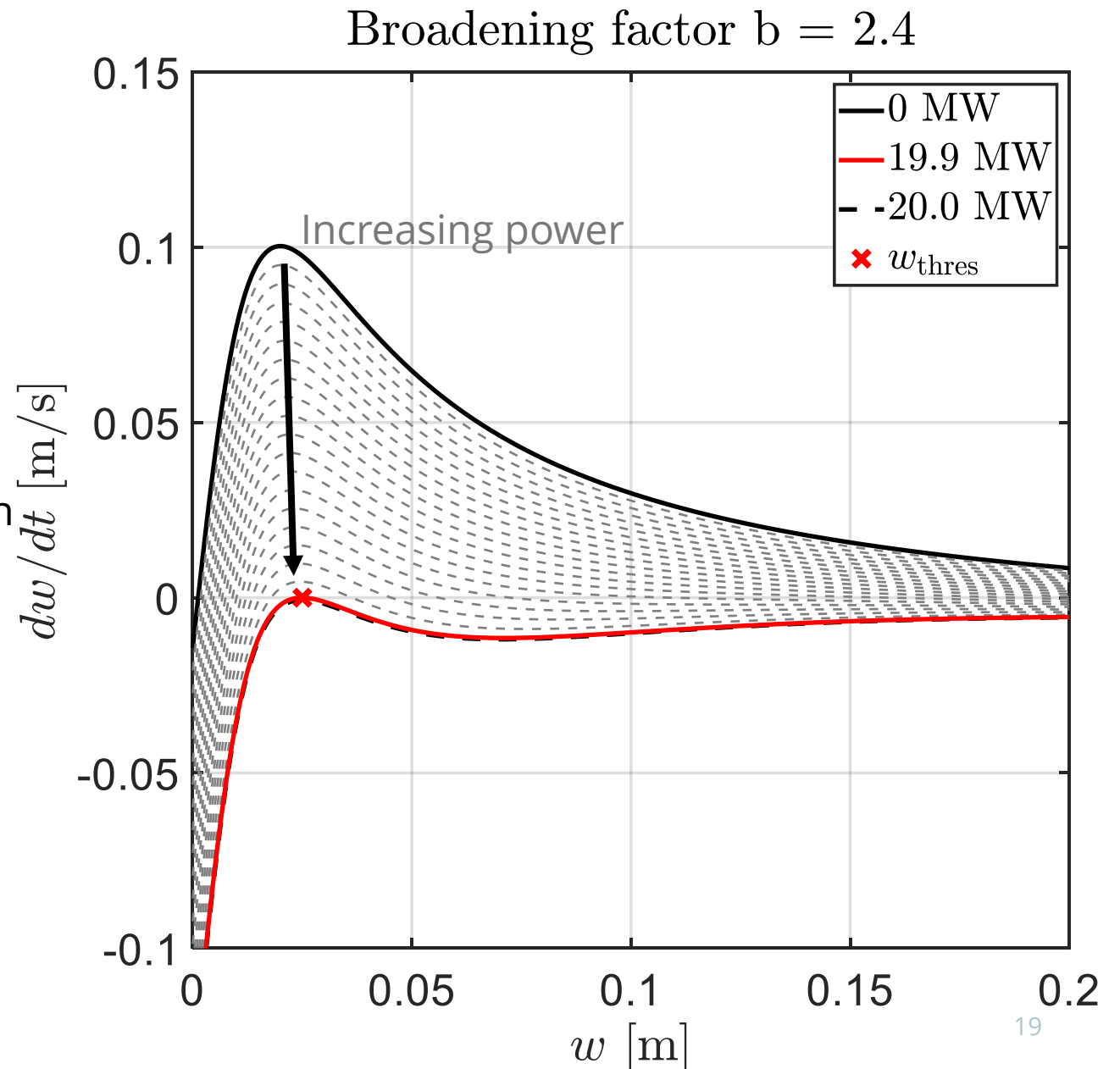
Results – Implications for ITER

- Estimation of P in DIII-D: factor 1.5 – 3 broadening with respect to ray-tracing^[1]
- No broadening: business-as-usual



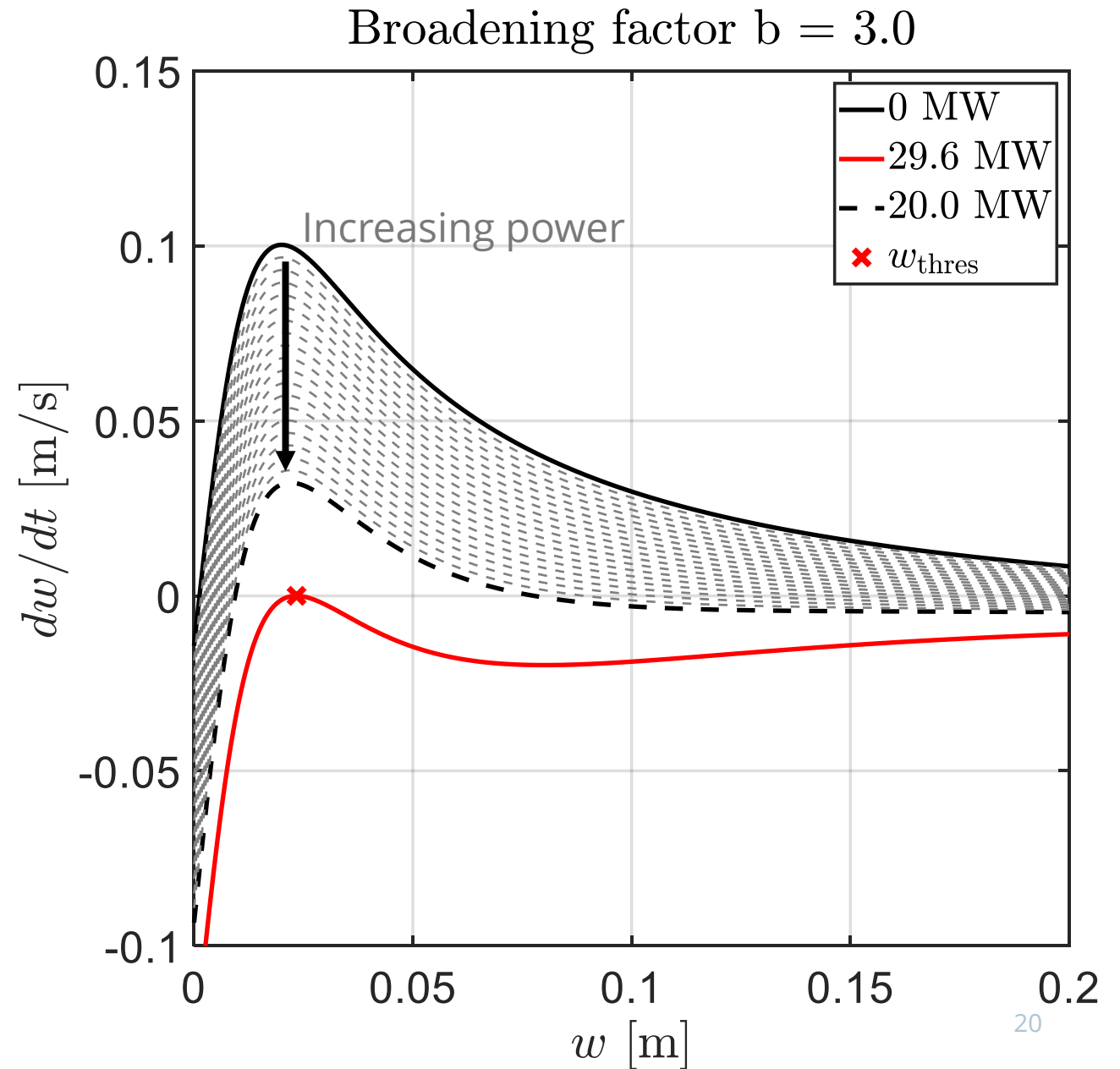
Results – Implications for ITER

- Estimation of P in DIII-D: factor 1.5 – 3 broadening with respect to ray-tracing^[1]
- Edge case at factor 2.4 broadening: all available power required for suppression



Results – Implications for ITER

- Estimation of P in DIII-D: factor 1.5 – 3 broadening with respect to ray-tracing^[1]
- At factor 3 broadening, more power required than available



Conclusions & Outlook

- Several methods can **simultaneously estimate any combination of D,V,K,P**
- **Key assumptions hold** in relevant experimental conditions
- **Coefficients have different sensitivities** to errors in the others
- Temperature profile sensitivity is **modulation frequency dependent**
- **Significant broadening in DIII-D P** estimates
- This could have **consequences for ITER NTM control**

Outlook:

- Joint transport coefficient estimation
- Time varying effects using Kalman filters